

**IQ MODULATION SYSTEMS AND METHODS THAT USE SEPARATE
PHASE AND AMPLITUDE SIGNAL PATHS AND PERFORM
MODULATION WITHIN A PHASE LOCKED LOOP**

Cross Reference to Related Applications

This application is a Continuation-in-Part (CIP) of Application Serial No.
09/_____, filed October 31, 2000, entitled *IQ Modulation Systems and Methods
That Use Separate Phase and Amplitude Signal Paths*, assigned to the assignee of the
5 present invention, the disclosure of which is hereby incorporated herein by reference.

Field of the Invention

This invention relates to modulation systems and methods, and more
particularly to IQ modulation systems and methods.

Background of the Invention

Modulation systems and methods are widely used in transmitters to modulate
information including voice and/or data onto a carrier. The carrier may be a final
carrier or an intermediate carrier. The carrier frequency can be in UHF, VHF, RF,
15 microwave or any other frequency band. Modulators also are referred to as "mixers"
or "multipliers". For example, in a wireless communications terminal such as a
mobile radiotelephone, a modulator can be used for the radiotelephone transmitter.

Figure 1 illustrates a conventional IQ modulator. As shown in Figure 1, an IQ
modulator 110, also referred to as a "quadrature modulator" or a "quadrature
20 modulator", includes a quadrature splitter 120, also known as a 90° phase shifter, and
a pair of multipliers 116a, 116b coupled to the quadrature splitter. A controlled
oscillator 115, such as a Voltage Controlled Oscillator (VCO), is coupled to the
quadrature splitter 120 to produce 90° phased shifted oscillator signals. In-phase (I)
data 111a and quadrature-phase (Q) data 111b are coupled to a respective multiplier
25 or mixer 116a, 116b. Digital input data is converted to analog data by I Digital-to-
Analog Converter (DAC) 114a and Q DAC 114b, respectively. The outputs of the

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respective DACs 114a and 114b are applied to the respective low pass filters 112a and 112b to provide the respective I and Q data inputs 111a and 111b. The modulator 110 modulates the input data on a carrier by summing the outputs of the multipliers 116a, 116b at a summing node 118. The modulated carrier 113 is amplified by a power amplifier 122 and transmitted via an antenna 124.

In modern wireless communications, wireless communications terminals such as mobile radiotelephones continue to decrease in size, cost and/or power consumption. In order to satisfy these objectives, it generally is desirable to provide IQ modulation systems and methods that can provide high power modulation while reducing the amount of battery power that is consumed. Unfortunately, the power amplifier 122 of an IQ modulator may consume excessive power due to efficiency limitations therein. More specifically, it is known to provide a linear class-A or class-AB power amplifier 122 that may have efficiencies as low as 30 percent or less. Thus, large amounts of battery power may be wasted as heat. Moreover, the noise figure of a conventional IQ modulator may be excessive so that high cost Surface Acoustic Wave (SAW) filters may need to be used.

Figure 2 illustrates other conventional modulation systems. As shown in Figure 2, I-data and Q-data is modulated on an Intermediate Frequency (IF) signal supplied by a controlled oscillator such as a voltage controlled oscillator 202 by applying the I-data and Q-data and the output of the IF voltage controlled oscillator 202 to an IQ modulator 204. The output of the modulator is then bandpass filtered by an IF bandpass filter 206. A local oscillator 212 and an up-conversion mixer 214 are used to up-convert the output of the bandpass filter 206 to a desired radio frequency. The output of the up-conversion mixer 214 is bandpass filtered by a radio frequency bandpass filter 216 to reduce noise and spurious levels. The filtered signal is then amplified using a variable gain amplifier 222 to provide the appropriate signal level to a power amplifier 226 which delivers the signal to an antenna 232 via a duplex filter 234. Additional RF bandpass filtering 224 may be used between the variable gain amplifier 222 and the power amplifier 226.

Figure 3 is a block diagram of other conventional modulation systems wherein like elements to Figure 2 are labeled with like numbers. The approach shown in Figure 3 is similar to that of Figure 2 except the IF signal is up-converted to the RF band first and then modulated in the IQ modulator 204.

Unfortunately, in either of the conventional approaches of Figures 2 or 3, the IQ modulator 204, up-conversion mixer 214 and/or the variable gain amplifier 222 may generate significant amounts of additive noise and spurious levels which may need to be filtered before the signal reaches the power amplifier 226. Systems of
 5 Figures 2 and 3 also may suffer from high current consumption and may need to use an excessive number of filters to meet the desired output spurious level and desired noise level.

It also is known to separately modulate the amplitude and phase of an input signal using an "rTheta" technique. In the rTheta technique, the phase is modulated at
 10 the oscillator, and the amplitude is modulated at the power amplifier stage. Unfortunately, the rTheta technique may require the oscillator phase locked loop to support the phase modulation bandwidth. With wide bandwidth radiotelephone signals such as TDMA and CDMA signals, it may be increasingly difficult to provide the requisite bandwidth in the oscillator phase locked loop.

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Summary of the Invention

Embodiments of the present invention provide modulation systems and methods having separate phase and amplitude signal paths. In particular, according to
 20 embodiments of the present invention, a digital signal processor generates in-phase, quadrature-phase and amplitude signals from a baseband signal. A modulator modulates the in-phase and quadrature-phase signals to produce a modulated signal. A phase locked loop is responsive to the modulated signal. The phase locked loop includes a controlled oscillator having a controlled oscillator input. An amplifier includes a signal input, an amplitude or gain control input and an output. The signal
 25 input is responsive to the controlled oscillator output and the amplitude control input is responsive to the amplitude signal.

In other embodiments according to the present invention, the in-phase and quadrature-phase signals are normalized in-phase and quadrature-phase signals. In
 30 these embodiments, the digital signal processor generates the normalized in-phase signal as a respective sine or cosine of an angle theta and generates the normalized quadrature-phase signal as a respective cosine or sine of the angle theta, where theta is an angle whose tangent is the quadrature-phase signal divided by the in-phase signal. The amplitude signal also is normalized and is generated as the square root of the sum of the in-phase signal squared and the quadrature-phase signal squared.

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In other embodiments, the modulator is a first modulator and the modulated signal is a first modulated signal. These embodiments further comprise a second modulator that is responsive to the controlled oscillator output to produce a second modulated signal wherein the phase locked loop also is responsive to the second modulated signal. Moreover, in other embodiments a power control signal also is provided and the amplitude control input is responsive to the amplitude signal and to the power control signal.

In yet other embodiments, the phase locked loop that is responsive to the modulated signal includes a controlled oscillator having a controlled oscillator output and a feedback loop between the controlled oscillator input and the controlled oscillator output. The feedback loop includes a mixer that is responsive to a local oscillator. In these embodiments, the modulator may be placed in the phase locked loop. In some embodiments, the modulator may be placed in the feedback loop between the controlled oscillator output and the mixer, between the local oscillator and the mixer, or between the mixer and the controlled oscillator input. Thus, modulation may take place within the phased lock loop instead of, or in addition to, taking place prior to the phased lock loop.

Other modulation systems and methods according to embodiments of the invention include a quadrature modulator that modulates in-phase and quadrature-phase signals to produce a modulated signal. A phase tracking subsystem is responsive to the quadrature modulator to produce a phase signal that is responsive to phase changes in the modulated signal and that is independent of amplitude changes in the modulated signal. An amplitude tracking subsystem is responsive to the modulator to produce an amplitude signal that is responsive to amplitude changes in the modulated signal and that is independent of the phase changes in the modulated signal. An amplifier has a signal input, an amplitude control input and an output. The signal input is responsive to the phase signal and the amplitude control input is responsive to the amplitude signal.

In other embodiments, the phase tracking subsystem comprises a phase locked loop that is responsive to the modulated signal. The phase locked loop includes a controlled oscillator having a controlled oscillator output that produces the phase signal.

In other embodiments, the amplitude tracking system includes an automatic gain control subsystem that is responsive to the modulated signal to produce the

amplitude signal. In some embodiments, the automatic gain control subsystem comprises a first envelope detector that is responsive to the modulated signal, a second envelope detector that is responsive to the phase locked loop and a comparator that is responsive to the first and second envelope detectors to produce the amplitude signal. In yet other embodiments, the automatic gain control subsystem comprises a first envelope detector that is responsive to the modulated signal, a second envelope detector that is responsive to the amplifier and a comparator that is responsive to the first and second envelope detectors to produce the amplitude signal. In still other embodiments, the amplitude tracking system comprises an envelope detector that is responsive to the modulated signal to produce the amplitude signal.

In still other embodiments, the phase tracking system comprises a phase locked loop that is responsive to the modulated signal. The phased lock loop includes a controlled oscillator having a controlled oscillator input and a controlled oscillator output that produces the phase signal. The phase locked loop also includes a feedback loop between the controlled oscillator input and the controlled oscillator output. The feedback loop includes a mixer that is responsive to a local oscillator. The modulator is placed in the phase locked loop. In some embodiments, the modulator is placed in the feedback loop between the controlled oscillator output and the mixer, between the local oscillator and the mixer, or between the mixer and the controlled oscillator input. Accordingly, the modulation may take place within the feedback loop in addition to taking place before the phase locked loop.

In all of the above-described embodiments, an optional power amplifier may be included that is responsive to the output of the amplifier having a signal input, an amplitude control input and an output. Alternatively, a power amplifier itself may have the signal input, the amplitude control input and the output. A transmit antenna is responsive to the amplifier or power amplifier.

Moreover, in all of the above-described embodiments, the amplifier may include a variable gain amplifier and/or a power amplifier, at least one of which includes an amplitude control input that is responsive to the amplitude signal. When both a variable gain amplifier and a power amplifier are used, the variable gain amplifier may precede the power amplifier or the power amplifier may precede the variable gain amplifier, regardless of which one includes the amplitude control input. Additional variable gain amplifiers and/or power amplifiers also may be included in the amplifier.

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Figures 1-3 are block diagrams of conventional IQ modulators; and
Figures 4-22 are block diagrams of IQ modulation systems and methods

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The present invention now will be described more fully hereinafter with reference to the accompanying drawings, in which preferred embodiments of the invention are shown. This invention may, however, be embodied in many different forms and should not be construed as limited to the embodiments set forth herein. Rather, these embodiments are provided so that this disclosure will be thorough and complete, and will fully convey the scope of the invention to those skilled in the art. Like numbers refer to like elements throughout. It will be understood that when an element is referred to as being "between" other elements, it can be directly between the other elements or intervening elements may also be present. In contrast, when an element is referred to as being "directly between" other elements, there are no intervening elements present.

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modulator **204** and the variable gain amplifier **222** may run at high current levels, which can reduce the operating time and generate excessive heat for portable wireless communication terminals.

5 Embodiments of the present invention can reduce the output noise and/or spurious levels so that the need for additional filters may be reduced and preferably may be eliminated. Moreover, the current consumption of an IQ modulator can be reduced while still meeting a desired linearity.

10 Referring now to Figure 4, modulation systems and methods according to embodiments of the present invention are shown. As shown in Figure 4, these embodiments of modulation systems and methods **400** include a quadrature (IQ) modulator **420** that modulates in-phase and quadrature-phase signals, referred to as I-data and Q-data, that may be generated by a user interface **410** in response to user commands, to produce a modulated signal **422**. A phase tracking subsystem **430** is responsive to the quadrature modulator **420** to produce a phase signal **432** that is
15 responsive to phase changes in the modulated signal **422** and that is independent of amplitude changes in the modulated signal **422**. An amplitude tracking subsystem **440** also is included that is responsive to the modulator **420** to produce an amplitude signal **442** that is responsive to amplitude changes in the modulated signal and that is independent of phase changes in the modulated signal **422**. An amplifier **450** includes
20 a signal input, an amplitude or gain control input and an output. The signal input is responsive to the phase signal **432**. The amplitude control input is responsive to the amplitude signal **442** and the output is applied to a transmit antenna **470**, optionally via a power amplifier **460**. Alternatively, the amplifier **450** may be a power amplifier.

25 Referring now to Figure 5, other modulation systems and methods according to embodiments of the present invention are shown. As shown in Figure 5, these modulation systems and methods **500** include an IQ modulator **420**, a phase tracking subsystem **430'**, an amplitude tracking subsystem **440'**, an amplifier **450**, a power amplifier **460** and an antenna **470**. As shown, the transmitter carrier frequency is generated using a fundamental radio frequency controlled oscillator such as a voltage
30 controlled oscillator **532** which can have an extremely high signal-to-noise ratio, on the order of -165dBc/Hz at 45MHz away. The output signal level is controlled using an amplifier **450** such as a saturated variable gain amplifier. The information signal (I-data and Q-data) is first modulated on an IF signal using the IQ modulator **420**. The IF signal is generated by a separate fundamental controlled oscillator such as a

voltage controlled oscillator **510**. The modulated signal then is provided to separate amplitude and phase tracking subsystems in the form of amplitude and phase tracking loops **440'** and **430'**, respectively. The modulated IF signal **422** acts as a reference for amplitude and phase comparators in the two corresponding tracking loops **440'** and **430'**. The RF output signal from the amplifier **450** is mixed down to the IF frequency using a system local oscillator **534**. The VCO **532** is phase locked using the phase locked loop that includes dividers **535a**, **535b**, a phase-frequency detector or a phase detector **537**, a pair of low pass filters **538a** and **538b**, and a limiter **539**. This phase locked loop acts as the channel synthesizer for the transmitter. The output of the mixer **533** is low pass filtered via low pass filter **538b** and fed to the limiter **539** along with the modulated reference IF signal **534**.

In the phase tracking loop **430'**, optional RF dividers **535a** and **535b** are placed in the reference and compare arms of the phase-frequency detector **537** to divide by M and N respectively. Since practical implementation of phase-frequency detectors at high frequencies may be difficult, this can allow for the lowering of the comparison frequency and can have negligible effect on the phase comparison. It also will be understood that the dividers **535a** and **535b** may be set such that $M=N$, or $M=N=1$, or may be eliminated.

In the amplitude-tracking loop **440'**, a pair of matched envelope detectors **442a** and **442b** are used to compare the amplitude level of the down-converted IF signal or other signal from the phase locked loop to that of the modulated signal **422**. Good matching between the two envelope detectors **442a** and **442b** may be provided to reduce AM offsets in the loop. Also, an adjustable constant delay element **445** may be introduced in the amplitude tracking loop **440'** to match the total group delay for the amplitude and phase signals. If the total delay is not matched, the output signal may not have the desired modulation characteristics.

Since the output power level of the transmitter is controlled by the amplifier **450** (VGA1) over a wide range, the total loop gain may change for the amplitude and phase tracking loops. In the phase tracking loop, the limiter **539** and/or the limiting action of the phase detector **537** can maintain constant loop gain, while in the amplitude tracking loop **440'**, a separate variable gain amplifier **446** (VGA2) with the opposite gain versus control voltage slope as the amplifier **450** is used. As the gain of VGA1 **450** is reduced to reduce output signal level, the gain of VGA2 **446** may be increased by the same amount to keep the signal level into the matched envelope

detectors **442a**, **442b** nearly constant. Otherwise, the envelope detectors **442a**, **442b** may need to have good matching over a very large (>50dB) range of signal levels at the input. Such wide dynamic range envelope detectors may be difficult to implement. One additional potential advantage of embodiments of Figure 5 is that the

5 AM/PM distortion in VGA1 **450** is compensated in the phase tracking loop **430'**. This can help achieve low phase and amplitude error over a wide range of output power levels.

The output signals of the phase and amplitude detectors are filtered using low-pass filters **538a**, **444** which can have bandwidths large enough to pass the modulation

10 signal (baseband) but narrow enough to suppress noise and spurious levels outside the modulation bandwidth. In effect, the low-pass filters **538a**, **538b** and **444** in the phase and amplitude tracking loops **440'** and **430'** can act as bandpass filters on the RF transmit carrier signal with very narrow bandwidth (i.e., very high-Q). For example, for 30kHz modulation bandwidth (common to digital wireless phones), the low-pass

15 filter bandwidth can be less than 1MHz. Therefore, the low-pass filter in the loop can be equivalent to a bandpass filter centered at the transmit frequency (e.g., 825MHz) having a bandwidth of less than 1MHz ($Q > 825$). The noise and spurious levels outside the 1MHz bandwidth around the carrier are attenuated according to the attenuation characteristics of the low-pass filters in the tracking loops. Such low-pass

20 filters can be implemented with resistors and capacitors, and thus can eliminate the need for expensive, multiple SAW filters.

Direct amplitude modulation of power amplifiers (especially saturated class-D power amplifiers) may be known. Some embodiments of the invention can provide electrical isolation between the modulation loop and the antenna. For example,

25 embodiments of Figure 5 can utilize the power amplifier **460** as an isolator providing electrical isolation between the antenna **470** and the transmit modulator. In this case, the efficiency of the amplifier (VGA1) **450** may not be as important to the overall power consumption. Therefore, it can be easier to implement simultaneous AM modulation and large power control range in VGA1. The amplifier **450** can be

30 designed to operate in a fixed high-efficiency, linear mode without the need for dynamic bias adjustment. Alternatively, other embodiments can amplitude modulate the power amplifier itself. This can provide enhanced linearity margin and/or enhanced efficiency by utilizing a saturating power amplifier and restoring envelope amplitude through modulation of its supply.

Figure 6 depicts embodiments of the present invention in a half-duplex system such as a TDMA-only IS-136 terminal or an EDGE terminal. In this case, the signal-to-noise ratio of the transmitter can be high enough so that the duplexer filter 480 of Figure 5 can be replaced by a transmit-receive (T/R) switch 580 in the transmit path.

5 Also in Figure 6, the power amplifier 460 itself is amplitude modulated.

It also will be understood by those having skill in the art that in Figures 5 and 6, the input to the mixer 533 may be taken between the VCO 532 and the amplifier 450 rather than between the output of the amplifier 450 and the power amplifier 460 as illustrated.

10 Figure 7 is a block diagram of other modulation systems and methods according to embodiments of the invention. In these embodiments, the amplitude tracking subsystem 440" is implemented as a direct modulation or an open loop. This may be accomplished, for example, if an amplifier 450 having a linear voltage control characteristic is used. Such a circuit is feasible with integrated circuit design techniques. For embodiments of Figure 7, the divide ratio of the phase locked loop is
15 one so that M and N are set to 1 or no dividers 535a, 535b are used. The IF amplifier 746 after the down-converting mixer 533 can be either a variable gain amplifier or an AGC amplifier. This amplifier 746 may be used in order to reduce the input operating range of the limiter 539. The AM/PM distortion of the limiter 539 thereby can be
20 reduced. In Figure 7 the amplitude tracking subsystem 440" includes an envelope detector 742 such as a diode and an adjustable delay 445.

Figure 8 depicts embodiments that can be used in a half-duplex system such as a TDMA-only IS-136 terminal or an EDGE terminal. In Figure 8, the signal-to-noise ratio of the transmitter can be high enough so that the duplexer filter 480 can be
25 replaced by a transmit-receive (T/R) switch 580 in the transmit path that couples to a receiver amplifier 490.

It will be understood that if the phase-frequency detector 537 is difficult to implement as a low current standard integrated circuit solution then a standard active analog phase detector such as a Gilbert cell mixer can be used. Assisted acquisition
30 techniques then may be used to provide fast lock times for the PLL.

Figure 9 is a block diagram of modulation systems and methods according to other embodiments of the present invention. Figure 9 illustrates dual mode modulation systems and methods 900 that can produce cellular and PCS signals. As shown in Figure 9, a phase locked loop includes phase frequency detector or phase

detector 1140 and a low pass filter 1144a, 1144b and a controlled oscillator such as a VCO 1142a, 1142b for each mode. A main local oscillator 534 and a pair of mixers 533a, 533b also are provided. An amplitude tracking subsystem 440' also may be responsive to a power control signal 1110. A pair of variable gain amplifiers and/or power amplifiers 1150a, 1150b may be provided. A limiter 1120 also is provided between the modulator 420 and the phase frequency detector 1140.

In summary, embodiments of Figures 4-9 can deliver low-distortion complex modulation signals containing both amplitude and phase information, with very high signal-to-noise ratio (for example on the order of -165dBc/Hz at 45mHz offset) to a power amplifier. These embodiments can reduce or eliminate the need for SAW filters that are traditionally used in conventional digital radio transmitter architectures. They also can reduce power consumption and spurious products compared to the conventional up-mixing transmitters.

Referring now to Figure 10, a block diagram of other embodiments of modulation systems and methods according to the present invention is shown. As shown in Figure 10, these modulation systems and methods 1000 include a Digital Signal Processor (DSP) 920 that generates in-phase (I), quadrature-phase (Q) and amplitude (A) signals 922, 924 and 926, respectively, from a baseband signal 912 that may be generated by a user interface 910. A modulator such as an IQ modulator 930 modulates the in-phase and quadrature-phase signals 922 and 924, respectively, to produce a modulated signal 932. A phase locked loop 940 is responsive to the modulated signal. The phase locked loop 940 includes a controlled oscillator 942 having a controlled oscillator output 944. An amplifier 950 includes a signal input, an amplitude or gain control input and an output. The signal input is responsive to the controlled oscillator output 944 and the amplitude control input is responsive to the amplitude signal 926. An optional power amplifier 960 is responsive to the output of the amplifier 950. A transmit antenna is responsive to the power amplifier 960 and/or amplifier 950.

Figure 11 illustrates other modulation systems and methods 1100 according to embodiments of the present invention. As shown in Figure 11, the digital signal processor 920' generates in-phase I and quadrature-phase Q signals 923 and 925, respectively, from a baseband signal 912 at the input 921 thereof. A generator 928 within the digital signal processor 920' then generates normalized in-phase (I') and quadrature-phase (Q') signals 922' and 924' and a normalized amplitude signal 926'.

It will be understood that the generator 928 may be embodied as a hardware and/or software module in the digital signal processor 920', and that the signals 922', 924' and 926' may be generated directly from the baseband signal 912, without the need to generate the intermediate signals 923, 925. The normalized in-phase and quadrature signals 922' and 924' are applied to a modulator such as an IQ modulator 930, such that the modulated signal 936 is of constant amplitude, followed by a phase locked loop 940, amplifier 950, optional power amplifier 960 and antenna 970 as was described in connection with Figure 9. The normalized amplitude signal A' is applied to the gain control input of the amplifier 950.

Still referring to Figure 11, in embodiments of the invention, the digital signal processor 920' generates the normalized in-phase signal I' 922' as a cosine of an angle θ and generates the normalized quadrature-phase signal Q' 924' as a sine of the angle θ , where the angle θ is an angle whose tangent is the quadrature-phase signal 925 divided by the in-phase signal 923. Moreover, the normalized amplitude signal 926' is generated as the square root of the sum of the in-phase signal I 923 squared and the quadrature-phase signal Q 925 squared. It will be understood that the sine and cosine functions may be interchanged from that which is described above.

Embodiments of Figures 10 and 11 can mathematically manipulate I, Q and A signals to allow reduced distortion in modulators. Conventionally, I and Q signals come from the baseband section of a wireless terminal carrying the modulating information that represents a voice and/or data signal that is to be transmitted. I and Q signals also can be represented as amplitude and phase signals. As was already described, a conventional transmitter modulates a VCO with this I and Q information and then amplifies the composite signal and up-converts the frequency to the transmit frequency. In sharp contrast, embodiments of Figures 10 and 11 perform numerical generation of I, Q and A signals from baseband. Moreover, embodiments of Figure 11 generate normalized I, Q and A signals I', Q' and A', respectively, from baseband. This can eliminate the need for a limiter to inject the signals into the phase locked loop of an rTheta architecture. The amplitude signal A' may be generated numerically from baseband such that an envelope detector may not be needed for the analog reconstruction of that signal. Amplitude direct from baseband also can allow flexible phase shifting between amplitude and phase waveforms for rTheta architectures.

More particularly, conventional modulating systems, for example as illustrated in Figures 1, 2 and 3, generate amplitude information from the IQ signal so that the rest of the transmitter chain may need to be linear enough to meet desired modulation specifications. In contrast, if the amplifiers can be saturated instead of linear, current consumption may be reduced. Moreover, conventional modulation systems may have low levels of linearity for a given current consumption. This may be especially true for modulation schemes whose peak-to-average is not a fundamental limit and even further back-off may be needed to satisfy near channel interference levels.

Moreover, embodiments of Figure 9 may produce an amplitude control signal 442 that may not be ideal because of distortion caused in the IQ modulator 420. The amplitude tracking circuit 440'' also may cause distortion. It also may be generally desirable to place a limiter 1120 between the IQ modulator 420 and the phase locked loop to remove unwanted amplitude information. The limiter 1120 may cause AM/PM distortion in the phase signal 432a, 432b and also can cause unwanted delay between the amplitude and phase signals when they are combined at the driver stages 1150a and 1150b.

In contrast, embodiments of Figures 10 and 11 can calculate a desired output for an amplitude tracking subsystem 440 (Figure 4) and can apply this output directly. Moreover, a limiter may not be needed because limiting may already be incorporated into the generation of the I' and Q' signals.

Figure 12 is a block diagram of modulating systems and methods according to other embodiments of the present invention. As shown in Figure 12, a DSP 920' generates an I' signal 922', a Q' signal 924' and an A' signal 926' from a baseband signal 912. A controlled oscillator 910 and the I' and Q' signals 922' and 924', respectively, are applied to an IQ modulator 930 to produce a modulated signal 932 that is applied to a phase frequency detector or phase detector 940 including a pair of low pass filters 944a, 944b and a pair of controlled oscillators 942a, 942b. Also applied to the phase frequency detector 940 is a main local oscillator 990 modulated by second modulators 992a, 992b. The output of the controlled oscillators 942a, 942b are applied to amplifiers 950a and 950b, respectively, which can be variable gain amplifiers and/or other conventional amplifiers such as power amplifiers or driver amplifiers. As also shown in Figure 12, amplitude control also may be combined with a power control signal 982 in a combined power control and amplitude

control module 980. Accordingly, an improved rTheta architecture may be provided. Figure 13 is a block diagram of a single band version of Figure 12.

The following equations show how the I', Q' and A' signals may be calculated for embodiments of Figures 11, 12 and 13:

5
$$\theta = \tan^{-1}\left(\frac{Q}{I}\right)$$

The angle should be a four-quadrant representation of the I and Q-data.

$$I' = \cos \theta$$

$$Q' = \sin \theta$$

10 The I' and Q' signals also may be interchanged. Therefore, the I' and Q' signals can be used to modulate the IF, and can create an IF that can be identical to an IQ modulated IF signal that has passed through an ideal limiter. Since the I' and Q' signals can be free of amplitude information, a limiter may not be needed at the input of the phase-frequency detector of the phase locked loop. Phase distortion, or AM/PM distortion that may occur in a real limiter, also may be reduced or eliminated.

15 The A' signal is calculated as follows:

$$A' = \sqrt{I'^2 + Q'^2}$$

Since the A' signal is calculated mathematically and applied directly to the amplifier, it need not contain any of the distortion created in the IQ modulation of the IF, and it also need not contain any distortion from the amplitude detector circuit.

20 Accordingly, limiters/envelope detectors may be removed and related AM/PM distortion may be reduced or eliminated. VCO pulling also may be removed that may arise from amplitude variations on a phase only signal. Sending the amplitude directly from baseband can result in exact and repeatable power control, as well as flexibility in phase shifting of amplitude relative to phase only signals in rTheta transmitters.

25 Embodiments of the invention that were described in Figures 4-13 placed the quadrature modulator prior to the phase locked loop. Thus, for example, in Figures 4-8, the IQ modulator 420 modulates in-phase and quadrature phase signals, and provides a modulated signal 422 to a phase locked loop in a phase tracking system 430 or 430'. Similarly, in Figures 10-11, the IQ modulator 930 modulates I and Q signals and provides the modulated signal 932 to a phase locked loop 940. Thus, in

these embodiments, the IQ modulation may take place at the IF frequency by directly modulating the IF reference signal.

According to other embodiments that will be described below in connection with Figures 14-22, modulation is applied within the phase locked loop itself. In particular, the phase locked loop includes a controlled oscillator having a controlled oscillator input and a controlled oscillator output, and a feedback loop between the controlled oscillator input and the controlled oscillator output. The feedback loop includes a mixer that is responsive to a local oscillator. In some embodiments, the modulator is placed in the feedback loop between the controlled oscillator output and the mixer, between the local oscillator and the mixer, or between the mixer and the controlled oscillator input. Accordingly, the modulation can be applied by modulating a local oscillator signal and leaving the IF as an unmodulated signal. Alternatively, the modulation can be applied to the RF output, and then mixed with an unmodulated local oscillator and IF frequency. In yet another alternative, the modulation may be performed after the mixer in the feedback path of the phase locked loop if it is desired to keep the IQ modulator running at the IF frequency.

For example, Figure 14 is similar to Figure 4, except that the IQ modulator 420 is included within the phase tracking subsystem 430", preferably within the feedback loop of the phase locked loop of the phase tracking subsystem 430". Figure 15 is similar to Figure 10, except the IQ modulator 930 is included within the phase locked loop 940', preferably within the feedback loop thereof.

Figure 16 is a block diagram of embodiments of the invention that illustrate various alternative locations of the IQ modulator within the phase locked loop. It will be understood that Figure 16 can correspond to the phase tracking system 430 of Figure 4, 430' of Figures 5-8 and/or 430" of Figure 14, and/or the phase locked loop 940 of Figures 10-13, and/or 940' of Figure 15.

As shown in Figure 16, the phase locked loop 1600 includes a phase detector or phase-frequency detector 1620 that can correspond to the phase-frequency detector or phase detector 537 of Figures 5-8, 1140 of Figure 9 and/or 940 of Figures 12-13, and a low pass filter 1630 that can correspond to the low pass filter 538a of Figures 5-8, 1144a of Figure 9, and/or 944a of Figure 12. A controlled oscillator, such as a Voltage Controlled Oscillator (VCO) 1640 can correspond to the VCO 532 of Figures 5-8, 1142a, 1142b of Figure 9, 942a, 942b of Figure 12 and/or 942 of Figures 10, 11, 13 and 15. As also shown in Figure 16, the controlled oscillator has a controlled

oscillator input **1604** and a controlled oscillator output **1606**. A feedback loop **1602** is provided between the controlled oscillator output **1606** and the controlled oscillator input **1604** via the phase-frequency detector or phase detector **1620** and low pass filter **1630**. The feedback loop includes a mixer **1660** that can correspond to the mixer **533** of Figures 5-8, **533a**, **533b** of Figure 9, **922a**, **922b** of Figure 12 and/or **922** of Figure 13, and a local oscillator **1680** that can correspond to the local oscillator **534** of Figures 5-9 and/or **990** of Figures 12-13.

In Figure 16, four possible locations of the IQ modulator corresponding to IQ modulator **420** of Figures 4-9 and/or **930** of Figures 10-13 are shown by IQ modulators **1610**, **1650**, **1670** and **1690**. It will be understood by those having skill in the art that only one IQ modulator need be provided at only one of the positions shown in Figure 16. However, multiple IQ modulators also may be provided.

The IQ modulator **1610** is placed prior to the phase locked loop **1600** in a manner corresponding to Figures 4-13 as was described extensively above. The IQ modulator **1650** is placed in the feedback loop **1602** between the controlled oscillator output **1606** and the mixer **1660**. The IQ modulator **1670** is placed in the feedback loop **1602** between the local oscillator **1680** and the mixer **1660**. Finally, the IQ modulator **1690** is placed in the feedback loop **1602** between the mixer **1660** and the controlled oscillator input **1604**.

When the IQ modulator **1650** is placed between the output of the controlled oscillator **1606** and the mixer **1660**, the RF output signal of the controlled oscillator **1640** is modulated with the I and Q signals. Thus, this is an example of RF modulation. When the IQ modulator **1690** is placed between the mixer **1660** and the controlled oscillator input **1604**, this can correspond to IQ modulating at the IF frequency, but the modulation takes place in the feedback loop **1602** of the phase locked loop **1600**, rather than at the IF input, as would be the case with modulator **1610**. When the modulator **1670** is placed between the local oscillator **1680** and the mixer **1660**, the local oscillator frequency is modulated before it is mixed with the RF to create the IF feedback signal. The phase can be preserved through the mixer, so that an analogous situation to modulating with modulator **1610** may be provided.

It will be understood by those having skill in the art that each of the four positions of the modulators **1610**, **1650**, **1670** and **1690** shown in Figure 16 can provide the same result at the output. Various considerations may be used in deciding where to place the modulator. For example, it may be more efficient to IQ modulate

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at the IF frequency, so that modulators 1610 and 1690 may be preferred. Modulating at RF (modulator 1650) or at the local oscillator (modulator 1670) may consume more current than modulating at IF. However, the current consumption may depend on the frequency plan of the system. It also will be understood that an amplitude signal may be generated and/or applied in a manner that was described in any of the previous figures.

Figure 17 is a block diagram that is similar to Figure 5, except the IQ modulator 1650 is placed in the feedback loop between the output of the controlled oscillator 532 and the mixer 533, rather than the IQ modulator 420 of Figure 5. An IQ modulator 1670 or 1690 of Figure 16 also may be used in embodiments of Figure 17.

Figure 18 illustrates the use of an IQ modulator 1670 between the local oscillator 534 and the mixer 533, instead of the IQ modulator 420 at the input of the phase locked loop in Figure 6. It will also be understood that an IQ modulator 1650 or 1690 of Figure 16 also may be employed.

Figure 19 illustrates the use of an IQ modulator 1690 between the mixer 533 and the input of the controlled oscillator 532, instead of the IQ modulator 420 of Figure 7. It also will be understood that IQ modulators 1650 or 1670 also may be used. IQ modulators also may be used in the positions shown in Figure 16 in other embodiments of the invention according to Figures 8 and 9.

Figure 20 illustrates the use of a modulator 1650 between the output of the controlled oscillator 942 and the mixer 992, instead of the IQ modulator 930 of Figure 13. Figure 21 illustrates an IQ modulator 1670 between the local oscillator 990 and the mixer 992, instead of the IQ modulator 930 of Figure 13. Figure 22 illustrates an IQ modulator 1690 between the mixer 992 and the input of the controlled oscillator 942, instead of the IQ modulator 930 of Figure 13. Similar placements of the modulator may be provided for the embodiments of Figure 12.

In the drawings and specification, there have been disclosed typical preferred embodiments of the invention and, although specific terms are employed, they are used in a generic and descriptive sense only and not for purposes of limitation, the scope of the invention being set forth in the following claims.